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**Die folgenden Angaben sind den vom Anmelder eingereichten Unterlagen entnommen**

54 Verbundschichtplatten oder -folien und Formkörper daraus

57 Die Verbundschichtplatte oder -folie umfaßt

(1) eine Substratschicht, enthaltend, bezogen auf die Summe der Mengen der Komponenten A und B, und ggf. C und/oder D, die insgesamt 100 Gew.-% ergibt,

a 1-99 Gew.-% eines Pfropfcopolymerisats mit einer Pfropfgrundlage auf Basis eines C<sub>1-8</sub>-Alkylesters der Acrylsäure als Komponente A,

b 1-99 Gew.-% eines Copolymerisats als Komponente B,

c 0-80 Gew.-% Polycarbonate als Komponente C, und

d 0-50 Gew.-% faser- oder teilchenförmige Füllstoffe oder deren Gemische als Komponente D,

und

(3) eine Deckschicht aus Polymethylmethacrylat.

Vorzugsweise liegt zusätzlich zwischen der Deck- und der Substratschicht

(2) eine Zwischenschicht aus schlagzähmodifiziertem Polymethylmethacrylat, Polycarbonat oder einer Formmasse der Komponente (1) ohne Polycarbonat, wenn Komponente (1) Polycarbonat enthält, vor.

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100 Gew.-% ergeben, aufgebaut.

Komponente A ist ein Pfropfcopolymerisat aus

a1 1-99 Gew.-%, vorzugsweise 55-80 Gew.-%, insbesondere 55-65 Gew.-%, einer teilchenförmigen Pfropfgrundlage A1 mit einer Glasübergangstemperatur unterhalb von 0°C.

a2 1-99 Gew.-%, vorzugsweise 20-45 Gew.-%, insbesondere 35-45 Gew.-%, einer Pfropfauflage A2 aus den Monomeren, bezogen auf A2.

a21 40-100 Gew.-%, vorzugsweise 65-85 Gew.-%, Einheiten des Styrols, eines substituierten Styrols oder eines (Meth)acrylsäureesters oder deren Gemische, insbesondere des Styrols und/oder  $\alpha$ -Methylstyrols als Komponente A21 und

a22 bis 60 Gew.-%, vorzugsweise 15-35 Gew.-%, Einheiten des Acrylnitrils oder Methacrylnitrils, insbesondere des Acrylnitrils als Komponente A22.

Die Pfropfauflage A2 besteht dabei aus mindestens einer Pfropfhülle, wobei das Pfropfcopolymerisat A insgesamt eine mittlere Teilchengröße von 50-1000 nm aufweist.

Komponente A1 besteht dabei aus den Monomeren

a11 80-99,99 Gew.-%, vorzugsweise 95-99,9 Gew.-%, mindestens eines C<sub>1</sub>-g-Alkylesters der Acrylsäure, vorzugsweise n-Butylacrylat und/oder Ethylhexylacrylat als Komponente A11.

a12 0,01-20 Gew.-%, vorzugsweise 0,1-5,0 Gew.-%, mindestens eines polyfunktionellen vernetzenden Monomeren, vorzugsweise Diallylphthalat und/oder DCPA als Komponente A12.

Gemäß einer Ausführungsform der Erfindung beträgt die mittlere Teilchengröße der Komponente A 50-800 nm, vorzugsweise 50-600 nm.

Gemäß einer weiteren erfindungsgemäßen Ausführungsform ist die Teilchengrößenverteilung der Komponente A bimodal, wobei 60-90 Gew.-% eine mittlere Teilchengröße von 50-200 nm und 10-40 Gew.-% eine mittlere Teilchengröße von 50-400 nm aufweisen, bezogen auf das Gesamtgewicht der Komponente A.

Als mittlere Teilchengröße bzw. Teilchengrößenverteilung werden die aus der integralen Massenverteilung bestimmten Größen angegeben. Bei den erfindungsgemäßen mittleren Teilchengrößen handelt es sich in allen Fällen um das Gewichtsmittel der Teilchengrößen, wie sie mittels einer analytischen Ultrazentrifuge entsprechend der Methode von W. Scholtan und H. Lange, Kolloid-Z. und Z.-Polymere 250 (1972), Seiten 782-796, bestimmt wurden. Die Ultrazentrifugennmessung liefert die integrale Massenverteilung des Teilchendurchmessers einer Probe. Hieraus läßt sich entnehmen, wieviel Gewichtsprozent der Teilchen einen Durchmesser gleich oder kleiner einer bestimmten Größe haben. Der mittlere Teilchendurchmesser, der auch als d<sub>50</sub>-Wert der integralen Massenverteilung bezeichnet wird, ist dabei als der Teilchendurchmesser definiert, bei dem 50 Gew.-% der Teilchen einen kleineren Durchmesser haben als der Durchmesser, dem dem d<sub>50</sub>-Wert entspricht. Ebenso haben dann 50 Gew.-% der Teilchen einen größeren Durchmesser als der d<sub>50</sub>-Wert. Zur Charakterisierung der Breite der Teilchengrößenverteilung der Kautschukteilchen werden neben dem d<sub>50</sub>-Wert (mittlerer Teilchendurchmesser) die sich aus der integralen Massenverteilung ergebenden d<sub>10</sub>- und d<sub>90</sub>-Werte herangezogen. Der d<sub>10</sub>- bzw. d<sub>90</sub>-Wert der integralen Massenverteilung ist dabei entsprechend dem d<sub>50</sub>-Wert definiert mit dem Unterschied, daß sie auf 10 bzw. 90 Gew.-% der Teilchen bezogen sind. Der Quotient

$$\frac{d_{90} - d_{10}}{d_{50}} = Q$$

stellt ein Maß für die Verteilungsbreite der Teilchengröße dar. Als Komponente A erfindungsgemäß verwendbare Emulsionspolymerisate A weisen vorzugsweise Q-Werte kleiner als 0,5, insbesondere kleiner als 0,35 auf.

Bei den Acrylatkautschuken A1 handelt es sich vorzugsweise um Alkylacrylat-Kautschuke aus einem oder mehreren C<sub>1</sub>-g-Alkylacrylaten, vorzugsweise C<sub>4</sub>-g-Alkylacrylaten, wobei bevorzugt mindestens teilweise Butyl-, Hexyl-, Octyl- oder 2-Ethylhexylacrylat, insbesondere n-Butyl- und 2-Ethylhexylacrylat, verwendet wird. Diese Alkylacrylat-Kautschuke können bis zu 30 Gew.-% harte Polymere bildende Monomere, wie Vinylacetat, (Meth)acrylnitril, Styrol, substituiertes Styrol, Methylmethacrylat, Vinylether, einpolymerisiert enthalten.

Die Acrylatkautschuke enthalten weiterhin 0,01-20 Gew.-%, vorzugsweise 0,1-5 Gew.-%, an vernetzend wirkenden, polyfunktionellen Monomeren (Vernetzungsmonomere). Beispiele hierfür sind Monomere, die 2 oder mehr zur Copolymerisation befähigte Doppelbindungen enthalten, die vorzugsweise nicht in den 1,3-Stellungen konjugiert sind.

Geeignete Vernetzungsmonomere sind beispielsweise Divinylbenzol, Diallylmalat, Diallylfumarat, Diallylphthalat, Diethylphthalat, Triallylcyanurat, Triallylisocyanurat, Tricyclodecenylnylacrylat, Dihydrodicyclopentadienylnylacrylat, Triallylphosphat, Allylacrylat, Allylmethacrylat. Als besonders günstiges Vernetzungsmonomer hat sich Dicyclopentadienylnylacrylat (DCPA) erwiesen (vgl. DE-PC 12 60 135).

Bei der Komponente A handelt es sich um ein Pfropfcopolymerisat. Die Pfropfcopolymerisate A haben dabei eine mittlere Teilchengröße d<sub>50</sub> von 50-1000 nm, bevorzugt von 50-800 nm und besonders bevorzugt von 50-600 nm. Diese Teilchengrößen können erzielt werden, wenn man als Pfropfgrundlage A1 dieser Komponente A Teilchengrößen von 50-350 nm, bevorzugt von 50-300 nm und besonders bevorzugt von 50-250 nm verwendet.

Das Pfropfcopolymerisat A ist im allgemeinen ein- oder mehrstufig, d. h. ein aus einem Kern und einer oder mehreren Hüllen aufgebautes Polymerisat. Das Polymerisat besteht aus einer Grundstufe (Pfropfkern) A1 und einer oder mehreren darauf geptropften Stufen A2 (Pfropfauflage), den sogenannten Pfropfstufen oder Pfropfhüllen.

Durch einfache Pfropfung oder mehrfache schrittweise Pfropfung können eine oder mehrere Pfropfhüllen auf die Kautschukteilchen aufgebracht werden, wobei jede Pfropfhülle eine andere Zusammensetzung haben kann. Zusätzlich zu den pfropfenden Monomeren können polyfunktionelle vernetzende oder reaktive Gruppen enthaltende Monomere mit aufgeptropft werden (s. z. B. EP-A 230 282, DE-AS 36 01 419, EP-A 269 861).

In einer bevorzugten Ausführungsform besteht Komponente A aus einem mehrstufig aufgebauten Pfropfcopolymerisat, wobei die Pfropfstufen im allgemeinen aus harzbildenden Monomeren hergestellt sind und eine Glasübergangstemperatur T<sub>g</sub>

Copolymerisat. Der Anteil des Pfropfcopolymerisats A in dem bei der Pfropfcopolymerisation erhaltenen Polymerisationsprodukt wird nach der oben angegebenen Methode ermittelt.

Bei der Herstellung der Pfropfcopolymerisate A nach dem Emulsionsverfahren sind neben den gegebenen verfahrenstechnischen Vorteilen auch reproduzierbare Teilchengrößenveränderungen möglich, beispielsweise durch zumindest teilweise Agglomeration der Teilchen zu größeren Teilchen. Dies bedeutet, daß in den Pfropfcopolymerisaten A auch Polymere mit unterschiedlichen Teilchengrößen vorliegen können.

Vor allem die Komponente A aus Pfropfgrundlage und Pfropfhülle(n) kann für den jeweiligen Verwendungszweck optimal angepaßt werden, insbesondere in bezug auf die Teilchengröße.

Die Pfropfcopolymerisate A enthalten im allgemeinen 1-99 Gew.-%, bevorzugt 55-80 und besonders bevorzugt 55-65 Gew.-% Pfropfgrundlage A1 und 1-99 Gew.-%, bevorzugt 20-45, besonders bevorzugt 35-45 Gew.-% der Pfropfaufflage A2, jeweils bezogen auf das gesamte Pfropfcopolymerisat.

#### KOMPONENTE B

Komponente B ist ein Copolymerisat aus

b1 40-100 Gew.-%, vorzugsweise 60-85 Gew.-%, Einheiten des Styrols, eines substituierten Styrols oder eines (Meth)acrylsäureesters oder deren Gemische, insbesondere des Styrols und/oder  $\alpha$ -Methylstyrols als Komponente B1, b2 bis 60 Gew.-%, vorzugsweise 15-40 Gew.-%, Einheiten des Acrylnitrils oder Methacrylnitrils, insbesondere des Acrylnitrils als Komponente B2.

Gemäß einer bevorzugten Ausführungsform der Erfindung beträgt die Viskositätszahl der Komponente B 50-90, vorzugsweise 60-80.

Vorzugsweise ist Komponente B ein amorphes Polymerisat, wie es vorstehend als Pfropfaufflage A2 beschrieben ist. Gemäß einer Ausführungsform der Erfindung wird als Komponente B ein Copolymerisat von Styrol und/oder  $\alpha$ -Methylstyrol mit Acrylnitril verwendet. Der Acrylnitrilgehalt in diesen Copolymerisaten der Komponente B beträgt dabei 0-60 Gew.-%, vorzugsweise 15-40 Gew.-%, bezogen auf das Gesamtgewicht der Komponente B. Zur Komponente B zählen auch die bei der Pfropfcopolymerisation zur Herstellung der Komponente A entstehenden freien, nicht gepfropften Styrol/Acrylnitril-Copolymerisate. Je nach den bei der Pfropfcopolymerisation für die Herstellung des Pfropfcopolymerisats A gewählten Bedingungen kann es möglich sein, daß bei der Pfropfcopolymerisation schon ein hinreichender Anteil an Komponente B gebildet worden ist. Im allgemeinen wird es jedoch erforderlich sein, die bei der Pfropfcopolymerisation erhaltenen Produkte mit zusätzlicher, separat hergestellter Komponente B abzumischen.

Bei dieser zusätzlichen, separat hergestellten Komponente B kann es sich vorzugsweise um ein Styrol/Acrylnitril-Copolymerisat, ein  $\alpha$ -Methylstyrol/Acrylnitril-Copolymerisat oder ein  $\alpha$ -Methylstyrol/Styrol/Acrylnitril-Terpolymerisat handeln. Diese Copolymerisate können einzeln oder auch als Gemisch für die Komponente B eingesetzt werden, so daß es sich bei der zusätzlichen, separat hergestellten Komponente B beispielsweise um ein Gemisch aus einem Styrol/Acrylnitril-Copolymerisat und einem  $\alpha$ -Methylstyrol/Acrylnitril-Copolymerisat handeln kann. In dem Fall, in dem die Komponente B aus einem Gemisch aus einem Styrol/Acrylnitril-Copolymerisat und einem  $\alpha$ -Methylstyrol/Acrylnitril-Copolymerisat besteht, sollte vorzugsweise der Acrylnitrilgehalt der beiden Copolymerisate um nicht mehr als 10 Gew.-%, vorzugsweise nicht mehr als 5 Gew.-%, bezogen auf das Gesamtgewicht des Copolymerisats, voneinander abweichen. Die Komponente B kann jedoch auch nur aus einem einzigen Styrol/Acrylnitril-Copolymerisat bestehen, wenn bei den Pfropfcopolymerisationen zur Herstellung der Komponente A als auch bei der Herstellung der zusätzlichen, separat hergestellten Komponente B von dem gleichen Monomergemisch aus Styrol und Acrylnitril ausgegangen wird.

Die zusätzliche, separat hergestellte Komponente B kann nach den herkömmlichen Verfahren erhalten werden. So kann gemäß einer Ausführungsform der Erfindung die Copolymerisation des Styrols und/oder  $\alpha$ -Methylstyrols mit dem Acrylnitril in Masse, Lösung, Suspension oder wäßriger Emulsion durchgeführt werden. Die Komponente B hat vorzugsweise eine Viskositätszahl von 40 bis 100, bevorzugt 50 bis 90, insbesondere 60 bis 80. Die Bestimmung des Viskositätszahl erfolgt dabei nach DIN 53 726, dabei werden 0,5 g Material in 100 ml Dimethylformamid gelöst.

Das Mischen der Komponenten A und B und gegebenenfalls C, D, kann nach jeder beliebigen Weise nach allen bekannten Methoden erfolgen. Wenn die Komponenten A und B beispielsweise durch Emulsionspolymerisation hergestellt worden sind, ist es möglich, die erhaltenen Polymerdispersionen miteinander zu vermischen, darauf die Polymerisate gemeinsam auszufällen und das Polymerisatgemisch aufzuarbeiten. Vorzugsweise erfolgt jedoch das Abmischen der Komponenten A und B durch gemeinsames Extrudieren, Kneten oder Verwalzen der Komponenten, wobei die Komponenten, sofern erforderlich, zuvor aus der bei der Polymerisation erhaltenen Lösung oder wäßrigen Dispersion isoliert worden sind. Die in wäßriger Dispersion erhaltenen Produkte der Pfropfcopolymerisation (Komponente A) können auch nur teilweise entwässert werden und als feuchte Krümel mit der Komponente B vermischt werden, wobei dann während des Vermischens die vollständige Trocknung der Pfropfcopolymerisate erfolgt.

In einer bevorzugten Ausführungsform enthält die Komponente (1) neben den Komponenten A und B zusätzliche Komponenten C und/oder D, sowie ggf. weitere Zusatzstoffe, wie im folgenden beschrieben.

#### KOMPONENTE C

Geeignete Polycarbonate C sind an sich bekannt. Sie haben vorzugsweise ein Molekulargewicht (Gewichtsmittelwert  $M_w$ , bestimmt mittels Gelpermeationschromatographie in Tetrahydrofuran gegen Polystyrolstandards) im Bereich von 10 000 bis 60 000 g/mol. Sie sind z. B. entsprechend dem Verfahren der DE-B-13 00 266 durch Grenzflächenpolykondensation oder gemäß dem Verfahren der DE-A-14 95 730 durch Umsetzung von Diphenylcarbonat mit Bisphenolen erhältlich. Bevorzugtes Bisphenol ist 2,2-Di(4-hydroxyphenyl)propan, im allgemeinen wie auch im folgenden als Bisphenol A bezeichnet.

Anstelle von Bisphenol A können auch andere aromatische Dihydroxyverbindungen verwendet werden, insbesondere 2,2-Di(4-hydroxyphenyl)pentan, 2,6-Dihydroxynaphthalin, 4,4'-Dihydroxydiphenylsulfan, 4,4'-Dihydroxydiphenylet-

\* Das Mischen der z. B. trockenen Komponenten kann nach allen bekannten Methoden erfolgen. Vorzugsweise geschieht jedoch das Mischen durch gemeinsames Extrudieren, Kneten oder Verwalzen der Komponenten, bevorzugt bei Temperaturen von 180-400°C, wobei die Komponenten notwendigerfalls zuvor aus der bei der Polymerisation erhaltenen Lösung oder aus der wäßrigen Dispersion isoliert worden sind.

Dabei können die Komponenten gemeinsam oder getrennt/nacheinander eidosiert werden.

#### Schicht (2)

Schicht (2) ist eine Farbträger- bzw. Zwischenschicht. Eine Ausführungsform der Erfindung betrifft eine Verbundschichtplatte oder -folie aus einer wie vorstehend beschriebenen Substratschicht (1), Deckschicht (3) und einer dazwischen liegenden Zwischenschicht (2), die aus schlagzähem PMMA, Polycarbonat oder der vorstehend beschriebenen Komponente (1) aufgebaut ist, die kein Polycarbonat enthält, sofern die Substratschicht (1) Polycarbonat enthält. Weisen sowohl Substratschicht als auch Zwischenschicht entweder Polycarbonat auf oder sind polycarbonatfrei, so liegt ein Zweischichtaufbau vor.

Die Erfindung betrifft außerdem Verbundschichtplatten oder -folien, umfassend (2') eine Schicht aus schlagzähem PMMA, Polycarbonat oder der vorstehenden Komponente (1), und (3) eine Deckschicht aus PMMA. In diesem Fall kann die Schicht (2') die gleichen Komponenten wie die Zwischenschicht (2) aufweisen. Zusätzlich kann sie auch der Komponente (1) entsprechen, die Polycarbonat enthält.

Wird Polycarbonat als Zwischenschicht (2) oder als Schicht (2') verwendet, so kann das unter Komponente (1), Komponente C beschriebene Polycarbonat eingesetzt werden.

Schlagzähes PMMA (high impact PMMA: HI-PMMA) ist ein Polymethylmethacrylat, das durch geeignete Zusätze schlagzäh ausgerüstet ist. Geeignete schlagzähmodifizierte PMMA sind beispielsweise beschrieben von M. Stickler, T. Rhein in Ullmann's encyclopedia of industrial chemistry Vol. A21, Seiten 473-486, VCH Publishers Weinheim, 1992, und H. Domininghaus, Die Kunststoffe und ihre Eigenschaften, VDI-Verlag Düsseldorf, 1992. Die Zwischenschicht (2) oder die Schicht (2') kann farbgebende Stoffe enthalten. Dies sind beispielsweise Farbstoffe oder Pigmente. Dabei können die Farbstoffe oder Pigmente organische oder anorganische Verbindungen sein.

#### Schicht (3)

Schicht (3) der erfindungsgemäßen Verbundschichtplatten oder -folien ist eine Deckschicht aus PMMA. Das verwendete PMMA hat vorzugsweise ein Zahlenmittel des Molekulargewichts von 40.000 bis 100.000. Beispiele geeigneter PMMA-Formmassen sind Lucryl® G88 bzw. G87 der Resal/BASF, sowie die in der EP-A2-0 225 500 beschriebenen Massen.

Die Schichtdicke der vorstehenden Verbundschichtplatten oder -folien beträgt vorzugsweise 100 µm bis 10 mm. Verbundschichtplatten weisen dabei besonders bevorzugt eine Schichtdicke von 3 bis 10 mm auf. Verbundschichtfolien weisen besonders bevorzugt eine Schichtdicke von 100-500 µm auf.

Verbundschichtplatten aus einer Substratschicht (1), einer Zwischenschicht (2) bzw. einer Schicht (2') und einer Deckschicht (3) weisen vorzugsweise die folgenden Schichtdicken auf: Substratschicht (1) 3 bis 9,5 mm, besonders bevorzugt 3-7 mm, insbesondere 3-5 mm; Zwischenschicht (2) oder Schicht (2') 50 bis 500 µm, besonders bevorzugt 200 bis 400 µm; Deckschicht (3) 5-300 µm, besonders bevorzugt 20-100 µm. In einer besonders bevorzugten Ausführungsform hat die Substratschicht (1) eine Dicke von 3-4 mm, die Zwischenschicht (2) bzw. Schicht (2') eine Dicke von 200-300 µm und die Deckschicht (3) eine Dicke von 30-70 µm.

Diese Dreischichtplatte kann beispielsweise aus einer Verbundschichtfolie mit 2 Schichten (2') und (3) hergestellt werden, indem sie mit einer Substratschicht (1) versehen wird. Die Herstellung kann nach dem nachstehend beschriebenen Verfahren erfolgen. Dazu ist es vorteilhaft, daß das Größenverhältnis der MFI-Werte (melt flow index: Schmelzflußindex) der einzelnen Komponenten der Verbundschichtplatten oder -folien maximal 3 : 1, besonders bevorzugt maximal 2 : 1 beträgt. Somit beträgt der größte MFI-Wert einer der Komponenten (1), (2), (2'), (3), sofern sie in den jeweiligen Verbundschichtplatten oder -folien vorliegen, maximal das Dreifache, besonders bevorzugt maximal das Zweifache des niedrigsten MFI-Wertes. Hierdurch wird ein gleichmäßiges Fließverhalten aller in den Verbundschichtplatten oder -folien verwendeten Komponenten sichergestellt. Dieses aufeinander abgestimmte Fließverhalten ist insbesondere vorteilhaft bei den nachstehend beschriebenen Herstellungsverfahren.

#### Herstellverfahren der Verbundschichtplatten oder -folien

Die erfindungsgemäßen Verbundschichtplatten oder -folien können durch Adapter- oder Coextrusion der Komponenten hergestellt werden. Dabei werden die einzelnen Komponenten in Extrudern fließfähig gemacht und über spezielle Vorrichtungen so miteinander in Kontakt gebracht, daß die Verbundschichtplatten oder -folien mit der vorstehend beschriebenen Schichtfolge resultieren. Beispielsweise können die Komponenten durch eine Breitschlitzdüse coextrudiert werden. Dieses Verfahren ist in der EP-A2-0 225 500 erläutert.

Zudem können sie nach dem Adaptercoextrusionsverfahren hergestellt werden, wie es im Tagungsband der Fachtagung Extrusionstechnik "Coextrusion von Folien", 8./9. Oktober 1996, VDI-Verlag Düsseldorf, insbesondere Beitrag von Dr. Netze beschrieben ist. Dieses wirtschaftliche Verfahren kommt bei den meisten Coextrusionsanwendungen zum Einsatz.

Weiterhin können die erfindungsgemäßen Verbundschichtplatten und -folien durch Aufeinanderkaschieren von Folien oder Platten der Komponenten in einem beheizbaren Spalt hergestellt werden. Dabei werden zunächst Folien oder Platten der einzelnen Komponenten hergestellt. Dies kann nach bekannten Verfahren erfolgen. Sodann wird die gewünschte Schichtfolge durch entsprechendes Übereinanderlegen der Folien oder Platten hergestellt, worauf diese durch einen beheizbaren Walzenspalt geführt werden und unter Druck- und Wärmeeinwirkung zu einer Verbundschichtplatte oder -fo-

Die Erfindung wird nachstehend anhand von Beispielen näher erläutert.

In den Beispielen wurden coextrudierte Platten eingesetzt, in denen die Substratschicht 3,7 mm dick war. Die Zwischenschicht, sofern sie verwendet wurde, wies eine Dicke von 0,25 mm auf. Die Deckschicht wies eine Dicke von 0,05 mm auf.

Dabei kamen unterschiedliche Werkstoffe zum Einsatz, wie PMMA, ABS, HI-PMMA und Komponente (1). Komponente (1) ohne Polycarbonat bestand dabei aus einem teilchenförmigen Piropfcopolymerisat mit einer Piropfgrundlage, die aus n-Butylacrylat und einem Vernetzer aufgebaut war, und einer Piropfaufgabe aus Styrol- und Acrylnitrileinheiten. Das Piropfcopolymerisat lag in einer Matrix aus einem Styrol/Acrylnitril-Copolymerisat vor. Zudem wurde Komponente (1) auch mit einem Anteil an Polycarbonat als weiterer Matrix-Komponente eingesetzt.

Für die Verringerung der Durchstoßarbeit durch die Aufbringung der PMMA-Schichten ergaben sich, prozentual bezogen auf die Substratwerte, die nachstehend aufgeführten Werte. Dabei wurde sowohl auf die Deckseite als auch die Rückseite der coextrudierten Platten geschlagen. Die Ergebnisse sind in Tabelle 1 zusammengefaßt.

Tabelle 1

Änderung der Durchstoßarbeit durch PMMA-Schichten. Wert in %, bezogen auf die Durchstoßarbeit des Substrats

Platte aus	Deckseite	Rückseite
PMMA/HI-PMMA/ Komponente (1) mit Polycarbonat	70	51
PMMA/Komponente (1)/ Komponente (1) mit Polycarbonat	102	62
PMMA/Polycarbonat/ Komponente (1) mit Polycarbonat	84	50
PMMA/ABS	54	52

Aus den Ergebnissen der Tabelle 1 geht hervor, daß die erfindungsgemäßen Platten eine gegenüber den Substratwerten entweder erhöhte oder nur geringfügig verminderte Durchstoßarbeit aufweisen im Vergleich zu den auf ABS basierenden Platten.

Weiterhin wurde die Kältezähigkeit entsprechender coextrudierter Platten untersucht. Es wurde die Durchstoßarbeit bei minus 30°C bestimmt. Es ergaben sich die in der nachstehenden Tabelle 2 angegebenen Werte.

Tabelle 2

Platte aus	Durchstoßbarkeit [Nm] -30°C
PMMA/HI-PMMA/Komponente (1) mit Polycarbonat	21,3
PMMA/Komponente (1)/Komponente (1) mit Polycarbonat	26,3
PMMA/Polycarbonat/Komponente (1) mit Polycarbonat	31,7
PMMA/Komponente (1)	10,6
PMMA/ABS	6,8

Aus den Ergebnissen der Tabelle 2 geht hervor, daß die erfindungsgemäßen Platten eine deutlich höhere Durchstoßarbeit gegenüber den bekannten Platten mit ABS als Substrat aufweisen. Insbesondere der Dreischichtaufbau führt zu we-

6. Verfahren zur Herstellung von Verbundschichtplatten oder -folien nach einem der Ansprüche 1 bis 5 durch Adapter- oder Coextrusion der Komponenten (1) und/oder (2)/(2') und/oder (3).
7. Verfahren zur Herstellung von Verbundschichtplatten oder -folien nach einem der Ansprüche 1 bis 5 durch Aufeinanderkaschieren von Folien oder Platten der Komponenten (1) und/oder (2)/(2') und/oder (3) in einem beheizbaren Walzenspalt. 5
8. Verwendung von Verbundschichtplatten oder -folien nach einem der Ansprüche 1 bis 5 zur Herstellung von Formkörpern.
9. Verfahren zur Herstellung von Formkörpern aus den Verbundschichtplatten nach Anspruch 1, 2 oder einem auf diese Ansprüche zurückbezogenen Anspruch durch Thermoformen der Verbundschichtplatten.
10. Verfahren zur Herstellung von Formkörpern aus den Verbundschichtplatten oder -folien nach Anspruch 3 oder einem der auf Anspruch 3 zurückbezogenen Ansprüche durch Thermoformen der Verbundschichtplatten oder -folien und Hinterspritzen mit Komponente (1) gemäß Anspruch 1 oder einem Polyurethanschaum. 10
11. Formkörper aus verformten Verbundschichtplatten nach einem der Ansprüche 1, 2 oder einem auf diese Ansprüche zurückbezogenen Anspruch.
12. Formkörper aus verformten Verbundschichtplatten oder -folien nach Anspruch 3, die mit Polyurethan hinterspritzt sind. 15

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(54) **FEUILLES OU PELLICULES LAMINEES ET MOULAGES AINSI  
PRODUITS**  
(54) **LAMINATED SHEETS OR FILMS AND MOLDINGS THEREOF**

(57) La feuille ou la pellicule laminée comprend 1) une couche de substrat comprenant - par rapport à la somme des quantités des constituants A et B et, le cas échéant, C et/ou D, qui totalisent 100 % en poids, a) 1 - 99 % en poids d'un copolymère par greffage particulier comme constituant A, b) 1 - 99 % en poids d'un copolymère de : b1) 40 - 100 % en poids d'unités de styrène, de styrène substitué ou de (méth)acrylate, ou des mélanges de ces derniers, comme constituant B1, b2) jusqu'à 60 % en poids d'acrylonitrile ou de méthacrylonitrile comme constituant B2, comme constituant B, c) 0 - 80 % en poids de polycarbonates comme constituant C, et d) 0 - 50 % en poids de charges de nature fibreuse ou particulaire ou des mélanges de ces dernières comme constituant D, et 3) une couche supérieure transparente de poly(méthacrylate de méthyle).

(57) The laminated sheet or film comprises (1) a substrate layer comprising - based on the sum of the amounts of components A and B and, if used, C and/or D, which totals 100% by weight a) 1 - 99% by weight of a particular graft copolymer as component A, b) 1 - 99% by weight of a copolymer of b1) 40 - 100% by weight of units of styrene, a substituted styrene or a (meth)acrylate, or mixtures thereof, as component B1, b2) up to 60% by weight of acrylonitrile or methacrylonitrile as component B2, as component B, C) 0 - 80% by weight of polycarbonates as component C, and d) 0 - 50% by weight of fibrous or particulate fillers or mixtures thereof as component D, and (3) a transparent top layer of polymethyl methacrylate.



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5

**Abstract**

The laminated sheet or film comprises

- (1) a substrate layer comprising - based on the sum of the amounts of  
10 components A and B and, if used, C and/or D, which totals 100% by weight
- a 1 - 99% by weight of a particular graft copolymer  
as component A,
  - 15 b 1 - 99% by weight of a copolymer of
    - b1 40 - 100% by weight of units of styrene, a substituted styrene or a  
(meth)acrylate, or mixtures thereof, as component B1,
    - 20 b2 up to 60% by weight of acrylonitrile or methacrylonitrile as  
component B2,
  - as component B,
  - 25 c 0 - 80% by weight of polycarbonates as component C, and
  - d 0 - 50% by weight of fibrous or particulate fillers or mixtures  
thereof as component D,
- and
- 30 (3) a transparent top layer of polymethyl methacrylate.



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**Laminated sheets or films and moldings thereof**

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The invention relates to laminated sheets or films, to processes for their production, to their use for producing moldings, to processes for producing the moldings and to moldings thereof.

- 15 When plastics are used outdoors where they are subjected to weathering and, in particular, to UV radiation, high standards are required in terms of UV stability and weatherability. Especially when they are used in exterior bodywork parts in the automotive sector, high requirements are also set for other mechanical properties, such as the low-temperature  
20 impact strength, as well as for the visual quality. The processes and materials employed at present do not always meet these conditions.

Bodywork parts made from plastics are, for example, topcoated or mass-colored and clearcoated. Topcoating in this case requires high heat  
25 deformation resistance, which is a requirement met by only a few plastics. Mass coloring, especially using special-effect pigments, is very costly and in many cases lessens the mechanical properties of the substrate.

- 30 Instead of spray coating it is possible to use other coating processes, such as the backspraying technology. In this, coating films are produced by

roller coating or intaglio printing processes and are backsprayed or backmolded with support materials.

J.H.Schut in *Plastics World*, July 1996, pages 48 to 52 describes the use  
5 of such coating films in the production of automotive components.  
Polyvinylidene fluoride films and polyvinyl fluoride films are described  
which are employed in conjunction with ABS as substrates. Polyvinylidene  
fluoride/acrylate films are also mentioned. Thermoplastic olefins can also  
be employed as substrates. Production techniques specified are  
10 thermoforming, thermoforming in conjunction with injection molding, and  
injection molding alone.

EP-B1-0 361 823 describes films of this kind which consist of fluoro  
polymers or mixtures thereof with acrylates. They are backmolded with  
15 curable, filler-reinforced polyester compositions. The layers can also  
comprise acrylonitrile-butadiene-styrene (ABS) copolymers.

To date, all known backspraying films have been used only for effect finishes and multicolored decoration, since the films are very costly.

20

US-A 5,192,609 describes coating films for the roller coating of a  
thermoplastic support material. Films with up to six layers are applied to  
a substrate. Besides polyolefins, the substrates mentioned include ABS and  
polyvinyl chloride.

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The topmost layer used is a clear coating which consists of a polymeric,  
crosslinkable two-component mixture, based for example on polyols.

EP-B-0 522 240 describes multilayer polymer film laminates which have a  
30 top layer based on polyvinylidene fluoride or polymethyl methacrylate and

a substrate comprising a polyolefin. The coextrusion of the top layer with subsequent extrusion-coating with the support material or further layers is described.

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Another known bodywork material comprises coextruded sheets of polymethyl methacrylate (PMMA) and ABS. For example H. Kappacher, in Kunststoffe 86 (1996), pp. 388 to 392, describes coextruded PMMA/ABS laminated sheets. The bodywork parts are produced by  
10 coextrusion through a slot die to form sheets, which are subsequently thermoformed. In some applications, however, the thermal aging resistance of the ABS is inadequate. In order to protect the ABS or ABS/PC against UV light it is necessary to employ relatively thick UV-absorbing PMMA top layers. The impact strength can also be inadequate, lessened  
15 as it is by the brittle PMMA top layer. Furthermore, the surface gloss decreases sharply at draw ratios of 1:2 and above.

The coextrusion process using a slot die is described, for example, in EP-A2-0 225 500.

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It is an object of the present invention to provide laminated sheets or films and moldings thereof which are of superior UV stability and thermal aging resistance as compared with known sheets, films or moldings. Moreover, high draw ratios should be possible without  
25 detriment to the surface gloss. It should be possible to produce the moldings at favorable cost. The products, furthermore, should be of enhanced elongation at break, low-temperature impact strength and scratch resistance and of increased penetration resistance.

30 We have found that this object is achieved in accordance with the

invention by means of laminated sheets or films comprising

- 5 (1) a substrate layer comprising - based on the sum of the amounts of components A and B and, if used, C and/or D, which totals 100% by weight -

a 1 - 99% by weight of a graft copolymer of

10 a1 1 - 99% by weight of a particulate graft base A1 comprising the following monomers:

a11 80 - 99.99% by weight of at least one C<sub>1-8</sub>-alkyl ester of acrylic acid as component A11,

15 a12 0.01 - 20% by weight of at least one polyfunctional crosslinking monomer as component A12;

a2 1 - 99% by weight of a graft A2 comprising the following monomers, based on A2:

20 a21 40 - 100% by weight of units of styrene, a substituted styrene or a (meth)acrylate, or mixtures thereof, as component A21 and

25 a22 up to 60% by weight of units of acrylonitrile or methacrylonitrile as component A22;

30 the graft A2 consisting of at least one graft shell and the graft copolymer having a mean particle size of 50 - 1000 nm,

as component A,

b 1 - 99% by weight of a copolymer of

5 b1 40 - 100% by weight of units of styrene, a substituted  
styrene or a (meth)acrylate, or mixtures thereof, as  
component B1,

b2 up to 60% by weight of acrylonitrile or methacrylonitrile as  
10 component B2,

as component B,

c 0 - 80% by weight of polycarbonates as component C, and  
15

d 0 - 50% by weight of fibrous or particulate fillers or  
mixtures thereof as component D,

and

(3) a transparent top layer of polymethyl methacrylate.  
20

The object is also achieved by laminated films comprising, in this order,

(1') a substrate layer comprising a molding compound of  
component (1) as described above, ABS, polycarbonate,  
25 polybutylene terephthalate, polyethylene terephthalate,  
polyamide, polyetherimide, polyether ketone, polyphenylene  
sulfide, polyphenylene ether or blends thereof, having a  
layer thickness of from 90 to 990  $\mu\text{m}$ ,

30 (3') a transparent top layer comprising polymethyl methacrylate

(PMMA), high-impact polymethyl methacrylate (HI-PMMA),  
ABS, polycarbonate (PC), polyethylene terephthalate (PET),  
styrene-acrylonitrile copolymers (SAN), polyamide (PA),  
polyether sulfone (PES) or polysulfone (PSU), having a  
5 layer thickness of from 10 to 100  $\mu\text{m}$ ,

it being possible for the substrate layer to comprise  
colorants and comprising them if the substrate layer and the  
top layer are composed of the same molding compounds,  
10 and the overall thickness of the laminated film being from  
100 to 1000  $\mu\text{m}$ .

The novel laminated sheets or films and also the moldings produced  
therefrom are of better penetration resistance and/or low-temperature  
15 impact strength, scratch resistance and elongation at break than the known  
sheets, films and moldings and have better drawing properties with  
constant surface gloss. They are therefore particularly suitable for exterior  
use, where they are subject to UV radiation and the effects of weather.  
Use in the automotive sector is particularly appropriate.

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The individual layers and components of the laminated sheets or films are  
described below.

#### Layer (1)

25

Layer (1) is composed of the following components A and B and, if  
used, C and/or D, which total to 100% by weight.

Component A is a graft copolymer of

30

- a1 1 - 99% by weight, preferably 55 - 80% by weight, in particular 55 - 65% by weight, of a particulate graft base A1 having a glass transition temperature of below 0°C,
- 5 a2 1 - 99% by weight, preferably 20 - 45% by weight, in particular 35 - 45% by weight, of a graft A2 comprising the following monomers, based on A2:
- a21 40 - 100% by weight, preferably 65 - 85% by weight, of units of  
10 styrene, a substituted styrene or a (meth)acrylate or mixtures thereof, especially of styrene and/or  $\alpha$ -methylstyrene, as component A21, and
- a22 up to 60% by weight, preferably 15 - 35% by weight, of units of acrylonitrile or methacrylonitrile, especially acrylonitrile, as component  
15 A22.

The graft A2 here consists of at least one graft shell, the graft copolymer A overall having a mean particle size of 50 - 1000 nm.

20 Component A1 consists of the following monomers:

- a11 80 - 99.99% by weight, preferably 95 - 99.9% by weight, of at least one  $C_{1-8}$ -alkyl ester of acrylic acid, preferably n-butyl acrylate and/or ethylhexyl acrylate, as component A11,
- 25 a12 0.01 - 20% by weight, preferably 0.1 - 5.0% by weight, of at least one polyfunctional crosslinking monomer, preferably diallyl phthalate and/or DCPA, as component A12.

30 In one embodiment of the invention the mean particle size of component

A is 50 - 800 nm, preferably 50 - 600 nm.

In another novel embodiment the particle-size distribution of component A is bimodal, 60 - 90% by weight of the particles having a mean size of 50 - 200 nm and 10 - 40% by weight having a mean size of 50 - 400 nm, based on the overall weight of component A.

The mean particle size and particle-size distribution indicated comprise the figures determined from the integral mass distribution. In the case of the mean particle sizes according to the invention the figure is in all cases the weight-average particle size as determined by means of an analytical ultracentrifuge in accordance with the process of W. Scholtan and H. Lange, *Kolloid-Z. und Z.-Polymere* 250 (1972), 782-796. The ultracentrifuge measurement gives the integral mass distribution of the particle diameter of a sample. From this it is possible to derive what percentage of the particles, by weight, has a diameter equal to or less than a certain size. The mean particle diameter, also referred to as the  $d_{50}$  value of the integral mass distribution, is defined as that particle diameter below which lie 50% by weight of the particles. At that point, 50% by weight of the particles also have a greater diameter than the  $d_{50}$  value. The breadth of the particle-size distribution of the rubber particles is characterized using not only the  $d_{50}$  value (mean particle diameter) but also the  $d_{10}$  and  $d_{90}$  values resulting from the integral mass distribution. The  $d_{10}$  and  $d_{90}$  values of the integral mass distribution are defined as for the  $d_{50}$  value with the difference that they are related to 10 and 90% by weight, respectively, of the particles. The quotient



$$\frac{d_{90} - d_{10}}{d_{50}} = Q$$

is a measure of the breadth of distribution (scatter) of the particle size. For emulsion polymers A which can be used in accordance with the invention as component A, Q is preferably less than 0.5, in particular  
5 less than 0.35.

The acrylate rubbers A1 are preferably alkyl acrylate rubbers comprising one or more C<sub>1-8</sub>-alkyl acrylates, preferably C<sub>4-8</sub>-alkyl acrylates, using preferably - at least in part - butyl, hexyl, octyl or 2-ethylhexyl acrylate,  
10 especially n-butyl and 2-ethylhexyl acrylate. Up to 30% by weight of these alkyl acrylate rubbers can comprise, in copolymerized form, monomers which form hard polymers, such as vinyl acetate, (meth)acrylonitrile, styrene, substituted styrene, methyl methacrylate and vinyl ethers.

15 The acrylate rubbers additionally include 0.01 - 20% by weight, preferably 0.1 - 5% by weight, of polyfunctional monomers having a crosslinking action (crosslinking monomers). Examples thereof are monomers containing 2 or more copolymerizable double bonds, which are  
20 preferably not 1,3-conjugated.

Examples of suitable crosslinking monomers are divinylbenzene, diallyl maleate, diallyl fumarate, diallyl phthalate, diethyl phthalate, triallyl cyanurate, triallyl isocyanurate, tricyclodecenyl acrylate, dihydro-  
25 dicyclopentadienyl acrylate, triallyl phosphate, allyl acrylate and allyl methacrylate. A crosslinking monomer which has proven particularly favorable is dicyclopentadienyl acrylate (DCPA; cf. DE-C 12 60 135).

Component A is a graft copolymer. The graft copolymers A have a mean particle size  $d_{50}$  of 50 - 1000 nm, preferably 50 - 800 nm and, with particular preference, 50 - 600 nm. Such particle sizes can be obtained by using a graft base A1 of this component A having particle sizes of 50  
5 - 350 nm, preferably 50 - 300 nm and, with particular preference, 50 - 250 nm.

The graft copolymer A is generally a single- or multistage polymer, i.e. a polymer composed of a core and of one or more shells. The polymer  
10 consists of a base stage (graft core) A1 and of one or - preferably - more stages A2 (graft) grafted thereon, called the graft stages or graft shells.

By single grafting or multiple, stepwise grafting it is possible to apply  
15 one or more graft shells to the rubber particles, it being possible for each graft shell to have a different composition. In addition to the grafting monomers, polyfunctional, crosslinking monomers or monomers containing reactive groups can also be grafted on (see for example EP-A 230 282, DE-B 36 01 419, EP-A 269 861).

20 In a preferred embodiment, component A consists of a multistage graft copolymer, the graft stages being produced generally from resin-forming monomers and having a glass transition temperature  $T_g$  of more than 30°C, preferably more than 50°C. The purpose of the multistage structure  
25 is, inter alia, to obtain (partial) compatibility of the rubber particles A with the thermoplastic B.

Graft copolymers A are produced, for example, by grafting at least one of the monomers A2 listed below onto at least one of the graft bases or  
30 graft core materials A1 listed above.

According to one embodiment of the invention, the graft base A1 is composed of 15 - 99% by weight of acrylate rubber, 0.1 - 5% by weight of crosslinker and 0 - 49.9% by weight of one of the other monomers or rubbers indicated.

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Monomers suitable for forming the graft A2 are styrene,  $\alpha$ -methylstyrene, (meth)acrylates, acrylonitrile and methacrylonitrile, especially acrylonitrile.

According to one embodiment of the invention, crosslinked acrylate  
10 polymers having a glass transition temperature of below 0°C are used as the graft base A1. The crosslinked acrylate polymers should preferably have a glass transition temperature of below -20°C, in particular below -30°C.

15 In one preferred embodiment the graft A2 consists of at least one graft shell and the outermost graft shell thereof has a glass transition temperature of more than 30°C, where a polymer formed from the monomers of the graft base A2 would have a glass transition temperature of more than 80°C.

20

Suitable production processes for graft copolymers A are emulsion, solution, bulk or suspension polymerization. The graft copolymers A are preferably produced by free-radical emulsion polymerization in the presence of lattices of component A1 at temperatures of 20°C - 90°C  
25 using water-soluble or oil-soluble initiators, such as peroxodisulfate or benzyl peroxide, or with the aid of redox initiators. Redox initiators are also suitable for polymerization below 20°C.

Appropriate emulsion polymerization processes are described in DE-A 28  
30 26 925 and 31 49 358 and in DE-C 12 60 135.

The synthesis of the graft shells takes place preferably by the emulsion polymerization process, as is described in DE-A 32 27 555, 31 49 357, 31 49 358, 34 14 118. Defined establishment of the particle sizes of 50 - 1000 nm according to the invention is preferably effected in accordance with the processes described in DE-C 12 60 135 and DE-A 28 26 925, or Applied Polymer Science, Volume 9 (1965), page 2929. The use of polymers having different particle sizes is known, for example, from DE-A 28 26 925 and US-A 5 196 480.

According to the process described in DE-C 12 60 135 the graft base A1 is first of all produced by polymerizing the acrylate or acrylates used in accordance with one embodiment of the invention and the polyfunctional, crosslinking monomer, alone or together with the other comonomers, in an aqueous emulsion in a manner known per se at from 20 to 100°C, preferably from 50 to 80°C. The customary emulsifiers can be used, for example alkali metal salts of alkyl- or alkylarylsulfonic acids, alkyl sulfates, fatty alcohol sulfonates, salts of higher fatty acids having 10 to 30 carbons, or resin soaps. Use is preferably made of the sodium salts of alkylsulfonates or fatty acids of 10 to 18 carbons. In one embodiment the emulsifiers are employed in amounts of 0.5 - 5% by weight, in particular 1 - 2% by weight, based on the monomers that are employed for producing the graft base A1. It is usual to operate with a weight ratio of water to monomers of from 2 : 1 to 0.7 : 1. Polymerization initiators used are, in particular, the customary persulfates, such as potassium persulfate. It is also possible, however, to employ redox systems. The initiators are generally employed in amounts of 0.1 - 1% by weight, based on the monomers that are employed in producing the graft base A1. Further polymerization auxiliaries used can be the customary buffer substances by means of which pH values of preferably 6 - 9 are established, such as sodium bicarbonate and sodium

pyrophosphate, and also 0 - 3% by weight of a molecular weight regulator, such as mercaptans, terpinols or dimeric  $\alpha$ -methylstyrene.

The precise polymerization conditions, especially the nature, rate of  
5 addition and amount of the emulsifier, are determined within the ranges  
set out above and specifically in such a way that the resulting latex of  
the crosslinked acrylate polymer has a  $d_{50}$  value in the range of about 50  
- 1000 nm, preferably 50 - 600 nm, and with particular preference, in  
the range of 80 - 500 nm. The particle-size distribution of the latex  
10 should preferably be narrow.

Then, to produce the graft polymer A, according to one embodiment of  
the invention a monomer mixture of styrene and acrylonitrile is  
polymerized in a subsequent step in the presence of the resultant latex of  
15 the crosslinked acrylate polymer, the weight ratio of styrene to acrylo-  
nitrile in the monomer mixture being - in accordance with one  
embodiment of the invention - in the range from 100 : 0 to 40 : 60,  
preferably in the range from 65 : 35 to 85 : 15. It is advantageous to  
carry out this graft copolymerization of styrene and acrylonitrile onto the  
20 crosslinked polyacrylate polymer, used as graft base, again in aqueous  
emulsion under the customary conditions described above. The graft  
copolymerization can judiciously be effected in the same system as the  
emulsion polymerization for producing the graft base A1, with the  
possible addition if required of further emulsifier and initiator. The  
25 monomer mixture of styrene and acrylonitrile which is to be engrafted in  
accordance with one embodiment of the invention can be added to the  
reaction mixture all at once, in stages in a number of portions or,  
preferably, continuously during the polymerization. The graft  
copolymerization of the mixture of styrene and acrylonitrile in the  
30 presence of the crosslinking acrylate polymer is conducted so as to give a

degree of grafting of 1 - 99% by weight, preferably 20 - 45% by weight, especially 35 - 45% by weight, based on the overall weight of component A, in the graft copolymer A. Since the grafting yield in the graft copolymerization is not 100%, it is necessary in the graft  
5 copolymerization to employ a somewhat larger amount of the monomer mixture of styrene and acrylonitrile than that corresponding to the desired degree of grafting. Control of the grafting yield in graft copolymerization and thus of the degree of grafting of the finished graft copolymer A is familiar to the skilled worker and can be done by playing, inter alia, on  
10 parameters such as the metering rate of the monomers or the addition of regulator (Chauvel, Daniel, ACS Polymer Preprints 15 (1974), page 329 ff.). The emulsion graft copolymerization generally produces about 5 - 15% by weight, based on the graft copolymer, of free, ungrafted styrene/acrylonitrile copolymer. The proportion of the graft copolymer A  
15 in the polymerization product obtained in the graft copolymerization is determined by the method indicated above.

In the case of the production of graft copolymers A by the emulsion process, in addition to the given process advantages, reproducible changes  
20 in particle size are also possible, for example by at least partial agglomeration of the particles to form larger particles. This means that in the graft copolymers A it is also possible for there to be polymers having different particle sizes.

25 In particular, component A comprising graft base and graft shell(s) can be optimized for the particular intended application, especially in terms of the particle size.

The graft copolymers A generally contain 1 - 99% by weight, preferably  
30 55 - 80 and, with particular preference, 55 - 65% by weight of graft

base A1 and 1 - 99% by weight, preferably 20 - 45 and, with particular preference, 35 - 45% by weight of the graft A2, based in each case on the graft copolymer as a whole.

5 **COMPONENT B**

Component B is a copolymer comprising

b1 40 - 100% by weight, preferably 60 - 85% by weight, of units of  
10 styrene, a substituted styrene or a (meth)acrylate or mixtures thereof,  
especially of styrene and/or  $\alpha$ -methylstyrene, as component B1,

b2 up to 60% by weight, preferably 15 - 40% by weight, of units of  
acrylonitrile or methacrylonitrile, especially of acrylonitrile, as  
15 component B2.

In accordance with a preferred embodiment of the invention, the viscosity number of component B is 50 - 90, preferably 60 - 80.

20 Component B is preferably an amorphous polymer as described above as graft A2. In one embodiment of the invention a copolymer of styrene and/or  $\alpha$ -methylstyrene with acrylonitrile is used as component B. The acrylonitrile content of these component B copolymers is 0 - 60% by weight, preferably 15 - 40% by weight, based on the overall weight of  
25 component B. Component B also embraces the free, ungrafted styrene-acrylonitrile copolymers that are formed in the course of the graft copolymerization for producing component A. Depending on the conditions chosen for the graft copolymerization for producing the graft copolymer A it may be possible for a sufficient amount of component B to be formed  
30 during the graft copolymerization itself. In general, however, it will be

necessary to blend the products obtained in the graft copolymerization with additional, separately produced component B.

This additional, separately produced component B can preferably be a  
5 styrene/acrylonitrile copolymer, an  $\alpha$ -methylstyrene-acrylonitrile copolymer  
or an  $\alpha$ -methylstyrene-styrene-acrylonitrile terpolymer. These copolymers  
can be employed individually or else as a mixture for component B, so  
that the additional, separately produced component B may, for example,  
comprise a mixture of a styrene-acrylonitrile copolymer and of an  $\alpha$ -  
10 methylstyrene-acrylonitrile copolymer. Where component B consists of a  
mixture of a styrene-acrylonitrile copolymer and of an  $\alpha$ -methylstyrene-  
acrylonitrile copolymer, the acrylonitrile contents of the two copolymers  
preferably should not differ by more than 10% by weight, particularly  
preferably by not more than 5% by weight, based on the overall weight  
15 of the copolymer. Component B may, however, alternatively consist of  
only one single styrene-acrylonitrile copolymer, if the same monomer  
mixture of styrene and acrylonitrile was used as the starting material in  
the graft copolymerizations for producing component A and in the  
production of the additional, separately produced component B.

20

The additional, separately produced component B can be obtained by the  
conventional processes. Thus, according to one embodiment of the  
invention, the styrene and/or  $\alpha$ -methylstyrene can be copolymerized with  
the acrylonitrile in bulk, solution, suspension or aqueous emulsion.

25 Component B preferably has a viscosity number of from 40 to 100, more  
preferably from 50 to 90 and in particular from 60 to 80. This viscosity  
number is determined in accordance with DIN 53 726, dissolving 0.5 g  
of material in 100 ml of dimethylformamide.

30 The mixing of components A and B and, if used, C, D can be



performed in any desired manner by any known process. If components A and B have been produced, for example, by emulsion polymerization it is possible to mix the resulting polymer dispersions with one another, then to precipitate the polymers jointly and to work up the polymer mixture. Preferably, however, the blending of components A and B is done by conjoint extrusion, kneading or rolling of the components, the latter having been isolated if necessary beforehand from the aqueous dispersion or solution obtained in the polymerization. The graft copolymerization products (component A) obtained in aqueous dispersion can also be only partially dewatered and can be mixed in the form of moist crumbs with component B, complete drying of the graft copolymers then taking place in the course of mixing.

In a preferred embodiment component (1) comprises, in addition to components A and B, additional components C and/or D, with or without other additives, as described below.

### COMPONENT C

Suitable polycarbonates C are known per se. They preferably have a molecular weight (weight mean value  $M_w$ , determined by gel permeation chromatography in tetrahydrofuran against polystyrene standards) in the range from 10,000 to 60,000 g/mol. They are obtainable, for example, by the processes of DE-B-1 300 266 by interfacial polycondensation or by the process of DE-A-1 495 730 by reacting diphenyl carbonate with bisphenols. A preferred bisphenol is 2,2-di(4-hydroxyphenyl)propane, which is referred to generally - and below - as bisphenol A.

Instead of bisphenol A it is also possible to use other aromatic dihydroxy compounds, especially 2,2-di(4-hydroxyphenyl)pentane, 2,6-

dihydroxynaphthalene, 4,4'-dihydroxydiphenyl sulfone, 4,4'-  
dihydroxydiphenyl ether, 4,4'-dihydroxydiphenyl sulfide, 4,4'-  
dihydroxydiphenylmethane, 1,1-di(4-hydroxyphenyl)ethane, 4,4'-dihydroxy-  
biphenyl or dihydroxydiphenylcycloalkanes, preferably  
5 dihydroxydiphenylcyclohexanes or dihydroxyphenylcyclopentanes, especially  
1,1-bis(4-hydroxyphenyl)-3,3,5-trimethylcyclohexane, and also mixtures of  
the abovementioned dihydroxy compounds.

Particularly preferred polycarbonates are those based on bisphenol A or  
10 on bisphenol A together with up to 80 mol% of the abovementioned  
aromatic dihydroxy compounds.

It is also possible to use copolycarbonates according to US-A 3 737 409;  
of particular interest in this context are copolycarbonates based on  
15 bisphenol A and di(3,5-dimethyldihydroxyphenyl) sulfone, which are  
notable for high heat deformation resistance. It is also possible to employ  
mixtures of different polycarbonates.

The average molecular weights (weight mean value  $M_w$ , determined by  
20 gel permeation chromatography in tetrahydrofuran against polystyrene  
standards) of the polycarbonates C are, in accordance with the invention,  
in the range from 10,000 to 64,000 g/mol. They are preferably in the  
range from 15,000 to 63,000, in particular in the range from 15,000 to  
60,000 g/mol. This means that the polycarbonates C have relative solution  
25 viscosities in the range from 1.1 to 1.3, measured in 0.5% strength by  
weight solution in dichloromethane at 25°C, preferably from 1.15 to 1.33.  
The relative solution viscosities of the polycarbonates employed preferably  
differ by not more than 0.05, in particular not more than 0.04.

30 The polycarbonates C can be employed either in ground or in granulated

form. As component C they are present in amounts of 0 - 50% by weight, preferably of 10 - 40% by weight, based in each case on the overall molding composition.

- 5 The addition of polycarbonates leads inter alia to greater thermal stability and improved crack resistance of the sheets, films and moldings.

#### COMPONENT D

- 10 As component D, component (1) comprises 0 - 50% by weight, preferably 0 - 40% by weight, and in particular, 0 - 30% by weight of fibrous or particulate fillers or mixtures thereof, based in each case on component 1 as a whole. These are preferably products which are available commercially.

15

Reinforcing materials such as carbon fibers and glass fibers are commonly used in amounts of 5 - 50% by weight, based on component (1) as a whole.

- 20 The glass fibers used can be of E, A or C glass and are preferably already treated with a size and with an adhesion promoter. Their diameter is in general from 6 to 20  $\mu\text{m}$ . It is possible to employ both continuous fibers (rovings) and cut glass fibers (staple) with a length of 1 - 10  $\mu\text{m}$ , preferably 3 - 6  $\mu\text{m}$ .

25

It is also possible to add fillers or reinforcing materials such as glass beads, mineral fibers, whiskers, alumina fibers, mica, quartz flour and wollastonite.

- 30 Other possibilities for addition are metal flakes (e.g. aluminum flakes

from Transmet Corp.), metal powders, metal fibers, metal-coated fillers, for example nickel-coated glass fibers, and other additives which screen against electromagnetic waves. Particularly suitable are aluminum flakes (K 102 from Transmet) for EMI (electro-magnetic interference) purposes. The  
5 compositions can also be mixed with additional carbon fibers, carbon black, especially conductivity black, or nickel-coated C fibers.

The component (1) used in accordance with the invention may, furthermore, include further additives which are customary and typical for  
10 polycarbonates, SAN polymers and graft copolymers or mixtures thereof. Examples which may be mentioned of such additives are dyes, pigments, colorants, antistatics, antioxidants, stabilizers for enhancing the thermal stability, for increasing the light stability, for raising the resistance to hydrolysis and the chemical resistance, heat stabilizers, and especially the  
15 lubricants that are judicious for the production of shaped articles and moldings. The addition of these further additives can take place at any stage in the production process, but they are preferably added early on so as to allow for early exploitation of the stabilizing effects (or other special effects) of the additive. Heat stabilizers and antioxidants are  
20 usually metal halides (chlorides, bromides, iodides) derived from metals of group I of the Periodic Table of the Elements (such as Li, Na, K, Cu).

Appropriate stabilizers are the customary hindered phenols, but also vitamin E and compounds of analogous structure. Also suitable are HALS  
25 (hindered amine light stabilizers), benzophenones, resorcinols, salicylates, benzotriazoles such as Tinuvin® P (UV absorber 2-(2H-benzotriazol-2-yl)-4-methylphenol from CIBA) and other compounds. They are usually used in amounts of up to 2% by weight (based on the overall mixture).

30 Suitable lubricants and mold release agents are stearic acids, stearyl

alcohol, stearic esters and, generally, higher fatty acids, their derivatives and corresponding fatty acid mixtures having 12 - 30 carbon atoms. The amounts of these additives are in the range 0.05 - 1% by weight.

- 5 Other suitable additives are silicone oils, oligomeric isobutylene or similar substances, with customary amounts being 0.05 - 5% by weight. It is likewise possible to use pigments, dyes, optical brighteners, special-effect colorants, such as titanium dioxide, carbon black, iron oxides, phthalocyanines, quinacridones, perylenes, anthraquinones, and aluminum spangles.

10

Processing aids and stabilizers such as UV stabilizers, lubricants and antistatics are commonly used in amounts of 0.01 - 5% by weight.

Component (1) can be produced by processes known per se, by mixing  
15 the components. It may be advantageous to premix certain components. Also possible is the mixing of the components in solution and removal of the solvents.

Examples of suitable organic solvents are chlorobenzene, mixtures of  
20 chlorobenzene and methylene chloride or mixtures of chlorobenzene or aromatic hydrocarbons, for example toluene.

The solvent mixtures can be evaporated, for example, in evaporative extruders.

25

The dry components, for example, can be mixed by any known method. Mixing is preferably effected, however, by conjoint extrusion, kneading or rolling of the components, preferably at 180 - 400°C, the components having been isolated beforehand if necessary from the solution obtained  
30 during the polymerization or from the aqueous dispersion.

In this context, the components can be added together or separately/in succession.

In the novel laminated films layer (1') is a substrate layer which  
5 comprises a molding compound of component (1) as described above,  
ABS, polycarbonate, polybutylene terephthalate (PBT), polyethylene  
terephthalate, polyamide, polyetherimide (PEI), polyether ketone (PEK),  
polyphenylene sulfide (PPS), polyphenylene ether or blends thereof. The  
individual materials here are known, for example from H. Domininghaus,  
10 Die Kunststoffe und ihre Eigenschaften [Plastics and their properties],  
VDI-Verlag, Dusseldorf (1992). The substrate layer preferably comprises a  
molding compound of component (1), ABS, polycarbonate, polybutylene  
terephthalate, polyethylene terephthalate, polyamide or blends thereof. It  
may also consist substantially or entirely of these polymers. With  
15 particular preference the substrate layer (1') comprises a molding  
compound of component (1), ABS, polycarbonate or polybutylene  
terephthalate, especially a molding compound of component (1). It may  
also consist substantially or entirely of these polymers.

20 The layer thickness is preferably 100 to 1000  $\mu\text{m}$ , in particular 200 to  
500  $\mu\text{m}$ .

#### **Layer (2)**

25 Layer (2) is a color backing layer or interlayer. One embodiment of the  
invention relates to a laminated sheet or film comprising a substrate layer  
(1) as described above, a top layer (3) and - in between them - an inter-  
layer (2) which is composed of toughened PMMA, polycarbonate or the  
above-described component (1) and which contains no polycarbonate if the  
30 substrate layer (1) contains polycarbonate. If both substrate layer and

interlayer either contain polycarbonate or are polycarbonate-free, then a two-layer structure is present.

The invention additionally relates to laminated sheets or films comprising

5

(2') a layer of toughened PMMA, polycarbonate or the above component (1) and

(3) a top layer of PMMA. In this case the layer (2') can have the same components as the interlayer (2). In addition, it may also correspond to component (1) containing polycarbonate.

10

If polycarbonate is used as interlayer (2) or as layer (2'), then it is possible to employ the polycarbonate described under component (1), component C.

15

Toughened PMMA (high-impact PMMA: HI-PMMA) is a polymethyl methacrylate which has been made impact-resistant by means of suitable additives. Suitable impact-modified PMMAs are described, for example, by M. Stickler, T. Rhein in Ullmann's encyclopedia of industrial chemistry Vol. A21, pages 473-486, VCH Publishers Weinheim, 1992, and by H. Domininghaus, Die Kunststoffe und ihre Eigenschaften, VDI-Verlag Düsseldorf, 1992. The interlayer (2) or the layer (2') can comprise special-effect colorants. These are, for example, dyes, metal flakes or pigments. The dyes or pigments can be organic or inorganic compounds.

20

25

The invention also relates to laminated films which between the substrate layer (1') and the transparent top layer (3') comprise

30

(2'') an interlayer of polymethyl methacrylate, high-impact polymethyl methacrylate, ABS, polycarbonate, polyethylene terephthalate, styrene-acrylonitrile copolymers, polyamide, polyether sulfone or polysulfone, which comprises special-effect colorants,

5

having a layer thickness of from 50 to 400, preferably from 100 to 300  $\mu\text{m}$ . The interlayer (2'') preferably has the same composition as the layer (2').

10 **Layer (3)**

Layer (3) of the laminated sheets or films according to the invention is a top layer of PMMA. The PMMA used preferably has a number-average molecular weight of from 40,000 to 100,000. Examples of suitable

15 PMMA molding compositions are Lucryl<sup>®</sup> G88 or G87 from Resart/BASF, and also the compositions described in EP-A2-0 225 500.

The layer thickness of the above laminated sheets or films is preferably from 100  $\mu\text{m}$  to 10 mm. Laminated sheets particularly preferably have a  
20 layer thickness of from 3 to 10 mm. Laminated films particularly preferably have a layer thickness of 100 - 500  $\mu\text{m}$ .

In the laminated films comprising the substrate layer (1') and, if used, the interlayer (2'') the transparent top layer (3') comprises polymethyl  
25 methacrylate, high-impact polymethyl methacrylate, ABS, polycarbonate, polyethylene terephthalate, styrene-acrylonitrile copolymers, polyamide, polyether sulfone or polysulfone, with a layer thickness of from 10 to 100  $\mu\text{m}$ .

30 It can also consist substantially or entirely of these polymers. The



transparent top layer (3') preferably comprises polymethyl methacrylate, high-impact polymethyl methacrylate, ABS, polycarbonate, polyethylene terephthalate or styrene-acrylonitrile copolymers. In particular it comprises polymethyl methacrylate, high-impact polymethyl methacrylate or  
5 polycarbonate, especially polymethyl methacrylate or high-impact polymethyl methacrylate. It may also consist substantially or entirely of these polymers. The polymers are chosen so that they result in a transparent top layer.

10 **Layer (0) .**

Layer (0) is an adhesion layer comprising an adhesion promoter having a layer thickness of from 5 to 100  $\mu\text{m}$ . It can be located on the outer surface of the substrate layer. The purpose of using the adhesion  
15 promoter is to produce a firm bond with a chosen substrate which comes to lie beneath the substrate layer (for example as a result of backspraying). The adhesion layer is used when the adhesion of this other substrate to the substrate layer is inadequate (for example in the case of polyolefin substrates). The adhesion promoter employed in this case is an  
20 adhesion promoter customarily employed for this combination of materials. Examples of suitable adhesion promoters are:

ethylene-vinyl acetate copolymers for coupling to polyethylene and maleic anhydride-grafted polypropylenes for coupling to polypropylene. In both  
25 cases, adhesion is achieved by the introduction of polar groups into the apolar polyolefins.

Laminated sheets comprising a substrate layer (1), an interlayer (2) or a layer (2') and a top layer (3) preferably have the following layer  
30 thicknesses: substrate layer (1) from 3 to 9.5 mm, particularly preferably

3 - 7 mm, especially 3 - 5 mm; interlayer (2) or layer (2') from 50 to 500  $\mu\text{m}$ , particularly preferably from 200 to 400  $\mu\text{m}$ ; top layer (3) 5 - 300  $\mu\text{m}$ , particularly preferably 20 - 100  $\mu\text{m}$ . In a particularly preferred embodiment the substrate layer (1) has a thickness of 3 - 4 mm, the  
5 interlayer (2) or layer (2') a thickness of 200 - 300  $\mu\text{m}$  and the top layer (3) a thickness of 30 - 70  $\mu\text{m}$ .

Laminated films comprising a substrate layer (1'), an interlayer (2'') if used, a top layer (3') and, if used, an adhesion layer (0) preferably have  
10 the following layer thicknesses:

substrate layer (1') 90 - 990  $\mu\text{m}$ ; interlayer (2'') 50 - 400  $\mu\text{m}$ ; top layer (3') 10 - 100  $\mu\text{m}$ ; adhesion layer (0) 5 - 100  $\mu\text{m}$ . The overall thickness of the laminated film in this case is 100 - 1000  $\mu\text{m}$ , preferably  
15 200 - 800  $\mu\text{m}$ .

The three-layer sheet can be produced, for example, from a laminated film having 2 layers (2') and (3) by providing it with a substrate layer (1). Production can be in accordance with the process described below.  
20 For this purpose it is advantageous for the ratio of the MFI (melt flow index) values of the individual components of the laminated sheets or films to be not more than 3:1, particularly preferably not more than 2:1. Consequently, the greatest MFI value of one of the components (0), (1), (1'), (2), (2'), (3), (3'), where present in the respective laminated sheets  
25 or films, is not more than three times, with particular preference not more than two times, the lowest MFI value. This ensures uniform flow properties of all of the components used in the laminated sheets or films. This harmonized flow behavior is particularly advantageous in the context of the production processes described below.

To protect the laminated sheets or films and moldings thereof in the course of production, transportation or processing it is possible to apply a transport protection film to the outside of the top layer (3) or (3') respectively. This film can be peeled off from the sheet or film after  
5 production, transportation or processing. The transport protection film can consist of any suitable material which can be separated from the top layer, examples being PET or polyolefin. Its layer thickness is preferably from 20 to 100  $\mu\text{m}$ . The transport protection film can be extruded on directly in the course of the production of the laminated sheets or films,  
10 or is laminated on.

#### **Processes for producing the laminated sheets or films**

The laminated sheets or films according to the invention can be produced  
15 by adapter extrusion or die coextrusion of the components. Adapter or die coextrusion takes place in particular with the components - where present - (0) and/or (1) and/or (1') and/or (2)/(2')/(2'') and/or (3)/(3'), the overall laminate being produced in a single-stage process.

20 In this case the individual components are rendered flowable in extruders and are brought into contact with one another by means of special equipment so as to give the laminated sheets or films having the layer sequence described above. For example, the components can be coextruded through a slot die. This process is explained in EP-A2-0 225  
25 500.

In addition, they can be produced by the adapter coextrusion process as described in the conference volume of the technical conference on extrusion technology "Coextrusion von Folien", October 8/9, 1996, VDI-  
30 Verlag Düsseldorf, in particular the paper by Dr. Netze. This economical

process is employed for the majority of coextrusion applications.

Furthermore, the laminated sheets and films according to the invention can be produced by laminating films or sheets of the components onto one another within a heatable nip. In particular, films or sheets of components (0) and/or (1)/(1') and/or (2)/(2") and/or (3)/(3') are laminated onto one another in a heatable roll nip. In this case, films or sheets of the individual components are produced first of all. This can be done by known processes. The desired layer sequence is then produced by laying the films or sheets over one another appropriately to form an assembly which is then passed through a heatable roll nip and laminated under the action of pressure and heat to form a laminated sheet or film.

Especially in the case of the adapter coextrusion process, harmonizing the flow properties of the individual components is advantageous for the development of uniform layers within the laminated sheets or films.

The laminated sheets or films can be used to produce any desired moldings. With particular preference the laminated sheets or films are used to produce moldings for which critical properties are a very good surface, high weatherability and good UV resistance. The surfaces, moreover, are highly scratch-resistant and firmly adhering, so that destruction of the surfaces by scratching or detachment of the surfaces is reliably prevented. Consequently, moldings for use in the exterior sector, out of doors, constitute a preferred field of application. The laminated sheets or films are employed in particular for producing automotive components, especially automotive components for exterior applications within the motor vehicle sector. Examples are the production of wings, door trims, fenders, spoilers, skirts and exterior mirrors.

The laminated sheets or films according to the invention are employed with particular advantage for producing colored moldings, especially moldings for exterior applications in the automotive field.

5 Moldings of laminated sheets that consist of a substrate layer (1) and a top layer (3) already have the very good surface properties mentioned above. To produce colored moldings, the substrate layer and if desired the top layer can be colored with color-imparting substances such as dyes or pigments. For producing colored moldings, the use of three-layer  
10 laminated sheets is of particular advantage. In this case it is sufficient to color only the interlayer (2) or, respectively, (2') or (2"). Coloring can again be carried out with all suitable color-imparting substances (colorants). In this case the top layer serves to protect the interlayer and to provide the desired surface properties. It is not necessary to color the  
15 voluminous substrate layer, with the result that very good coloring can be achieved with a small amount of colorant. As a result, it is also possible to use expensive colorants, since their concentration can be kept low. When using HI-PMMA and polycarbonate, in particular, as the interlayer it is possible to bring about depth (flop) effects. All other kinds of  
20 special coloration are also possible, such as metallic and effect finishes.

Moldings can be produced by known processes from the laminated sheets or films. For example, laminated sheets having the three-layer structure of substrate layer, interlayer and top layer or the two-layer structure of  
25 substrate layer and top layer can be produced by thermoforming, using either positive or negative thermoforming processes. Appropriate processes are known to the skilled worker. In such processes, the laminated sheets according to the invention are stretched or drawn. Since the gloss and the surface quality of the laminated sheets according to the invention does not  
30 decrease on stretching at high draw ratios, for example up to 1:5, there

are virtually no restrictions on the thermoforming processes in respect of the stretching possible.

From the laminated sheets or films composed of a layer (2') and a top  
5 layer (3) it is possible to produce moldings by thermoforming the  
laminated sheet or film and then backspraying (back-casting) with a  
component (1) or with a polyurethane foam. Thus the laminated sheet or  
film is first of all placed in the desired mold and then backsprayed. The  
films employed can also be referred to as backspraying films. By means  
10 of the thermoforming of backspraying films, followed by spraying, it is  
possible in particular to produce highly complex moldings. This process is  
also known as insert molding.

From the laminated films of the layers (0), (1') and, if used, (2") and  
15 (3') it is possible to produce moldings by backspraying or back-casting of  
the laminated films with component (1'), preferably ABS, PC/ASA,  
PC/PBT or else PP or PE in the case where an adhesion layer is used,  
or with a polyurethane foam, it being possible for the laminated film to  
be thermoformed beforehand, or by laminating a molding comprising one  
20 of the abovementioned components or a polyurethane foam with the  
laminated film.

The invention also relates to the moldings comprising shaped laminated  
sheets or films which may have been backsprayed. The moldings of the  
25 laminated sheets or films are backsprayed or back-cast with component  
(1') or with a polyurethane foam, or a molding of component (1') or a  
polyurethane foam is laminated with the laminated film.

In this case the moldings are preferably from the automotive sector, and  
30 in particular are exterior bodywork parts. They can be relatively small

automotive exterior bodywork parts, such as mirrors or trim strips, but can also be exterior bodywork parts of relatively large surface area, examples being wings, hoods, covers, doors and so on. They can also be fenders or bumpers. In this case, backspraying with polyurethane has the capacity, for example, to lead to fenders or bumpers having very good impact-damping properties.

The moldings can be used in general throughout the automotive sector.

10 The moldings according to the invention, especially in relation to moldings in which an ABS substrate layer is used, have the following advantages:

- 15 - lower loss in toughness of the PMMA top layer when the substrate layer according to the invention (component 1) is used, in comparison to the ABS substrate
- 20 - increased scratch resistance of the PMMA layer, which is also governed by the substrate layer lying below the top layer
- effective prevention of the formation of cracks in the PMMA top layer as a result of the toughened interlayer and/or toughened substrate layer
- 25 - thinner PMMA top layers can be used without reducing the UV stability of the substrate layer
- the moldings have very good properties in respect of low-temperature impact strength, elongation at break, scratch resistance and surface gloss
- 30

- the laminated sheets or films can be thermoformed with retention of gloss even at very high draw ratios (especially in the positive thermoforming process)
- 5 - cost-effective coloring is possible by coloring the thin interlayer
- depth (flop) effects can be produced in the interlayer, especially when it comprises HI-PMMA or polycarbonate
- 10 - cost-effective production by the adapter coextrusion process is possible, especially when the components selected have similar flow properties
- even highly viscous and scratch-resistant PMMA grades can be
- 15 coextruded with other highly viscous components
- moldings comprising polycarbonates in the substrate layer are highly resistant to thermal deformation and are particularly impact resistant
- 20 - no solvents are used in coloring with the laminated films.

The invention is illustrated in more detail below with reference to examples.

- 25 In the examples, coextruded sheets were employed in which the substrate layer was 3.7 mm thick. The interlayer, where used, had a thickness of 0.25 mm. The thickness of the top layer was 0.05 mm.

In these sheets various materials were employed, such as PMMA, ABS,

30 HI-PMMA and component (1). Component (1) without polycarbonate



consisted of a particulate graft copolymer having a graft base composed of n-butyl acrylate and a crosslinker, and a graft comprising styrene and acrylonitrile units. The graft copolymer was in a matrix comprising a styrene-acrylonitrile copolymer. In addition, component (1) was also  
5 employed with a proportion of polycarbonate as a further matrix component.

The values indicated below, as percentages based on the substrate values, were found for the reduction in the penetration energy as a result of  
10 applying the PMMA layers. Both the top face and the rear face of the coextruded sheets were tested by impact. The results are summarized in Table 1.

Table 1:

15

Change in the penetration energy as a result of PMMA layers, value in %, based on the penetration energy of the substrate

Sheet made of	Top face	Rear face
20 PMMA/HI-PMMA/component (1) with polycarbonate	70	51
PMMA/component (1)/ component (1) with polycarbonate	102	62
25 PMMA/polycarbonate/ component (1) with polycarbonate	84	50

PMMA/ABS	54	52
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The results of Table 1 show that the sheets according to the invention have a penetration energy which is either greater than or only slightly less than that of the substrates, comparison being with the sheets based on ABS.

The low-temperature impact strength of corresponding coextruded sheets was also investigated. The penetration energy was determined at -30°C, with the results shown in Table 2 below.

Table 2:

Sheet made of	Penetration energy [Nm] - 30°C
PMMA/HI-PMMA/component (1) with polycarbonate	21.3
PMMA/component (1)/component (1) with polycarbonate	26.3
PMMA/polycarbonate/component (1) with polycarbonate	31.7
PMMA/component (1)	10.6
PMMA/ABS	6.8

The results of Table 2 show that the sheets according to the invention have a markedly higher penetration energy than the known sheets having

ABS as substrate. The three-layer structure in particular leads to substantially higher low-temperature impact strengths.

A measurement was also made of the elongation at break under  
5 tensile/flexural loading. In this case the elongation at break was determined in the lengthwise (l) and crosswise (c) directions relative to the original direction of extrusion of the sheets. The results are given in Table 3 below.

Table 3:

Sheet made of	Elongation at break [%] l	Elongation at break [%] c
PMMA/PI-PMMA/component (1) with polycarbonate	5.9	4.3
PMMA/polycarbonate/ component (1) with polycarbonate	34.7	21.3
PMMA/component (1)/ component (1) with polycarbonate	8.1	8.1
PMMA/ABS	4.6	3.8

The results of Table 3 show that the elongation at break for the sheets according to the invention is substantially higher than for the comparison sheet.

The scratch resistance of the novel laminated films was also investigated, as follows:

using a scratch tester, each test sheet was marked with 10 scratches each 6 m in length at a distance of 1 mm from each other. This was done by moving a diamond tip with an acute angle of 120 degrees and a radius of 0.2 mm over the sample under a force of 2.6 N. Subsequently, the

surface topography normal to the direction of scratching was measured using a mechanical scanner (commercial Hommel tester). The depth of the marks, measured relative to the surface of the sample, is regarded as a measure of the scratch resistance.

5

The measurements were made at room temperature, with the results indicated in Table 4 below:

Table 4:

10

Laminated films	Scratch depth
PMMA/HI-PMMA (50 $\mu\text{m}$ /250 $\mu\text{m}$ )	0.5 $\mu\text{m}$
PMMA/ASA (50 $\mu\text{m}$ /450 $\mu\text{m}$ )	2.7 $\mu\text{m}$
PVDF film	5.5 $\mu\text{m}$

15

The results of Table 4 show that the scratch resistance for the laminated films according to the invention is substantially higher than for the PVDF film commonly employed.

20

In addition, the surface gloss before and after weathering was measured, in accordance with DIN 67530. The results are indicated in Table 5 below.

25

Table 5

Sheet made of	unweathered	after 500 h
---------------	-------------	-------------

PMMA/MI-PMMA/ component	81.1	84.1
PMMA/component (1)	79.7	85.4
ABS	56.5	49.5
Component (1)	78.1	69.6

The results of Table 5 show that the sheets according to the invention exhibit a substantially better surface gloss than the sheets which do not have a top layer of PMMA.

## We claim:

5

## 1. A laminated sheet or film comprising

- 10 (1) a substrate layer comprising - based on the sum of the amounts of components A and B and, if used, C and/or D, which totals 100% by weight -
- a 1 - 99% by weight of a graft copolymer of
- 15 a1 1 - 99% by weight of a particulate graft base A1 comprising the following monomers:
- a11 80 - 99.99% by weight of at least one C<sub>1-8</sub>-alkyl ester of acrylic acid as component A11,
- 20 a12 0.01 - 20% by weight of at least one polyfunctional crosslinking monomer as component A12;
- a2 1 - 99% by weight of a graft A2 comprising the following monomers, based on A2:
- 25 a21 40 - 100% by weight of units of styrene, a substituted styrene or a (meth)acrylate, or mixtures thereof, as component A21 and
- 30 a22 up to 60% by weight of units of acrylonitrile or methacrylonitrile as component A22;

the graft A2 consisting of at least one graft shell and the graft copolymer having a mean particle size of 50 - 1000 nm,

as component A,

5

b 1 - 99% by weight of a copolymer of

b1 40 - 100% by weight of units of styrene, a substituted styrene or a (meth)acrylate, or mixtures thereof, as component B1,

10

b2 up to 60% by weight of acrylonitrile or methacrylonitrile as component B2,

as component B,

15

c 0 - 80% by weight of polycarbonates as component C, and

d 0 - 50% by weight of fibrous or particulate fillers or mixtures thereof as component D,

20

and

(3) a transparent top layer of polymethyl methacrylate.

2. A laminated sheet or film as claimed in claim 1, additionally comprising between the top layer and the substrate layer

25

(2) an interlayer of impact-modified polymethyl methacrylate, polycarbonate or a molding composition of component (1) as set forth in claim 1 without polycarbonate, if component (1) contains polycarbonate.

30



3. A laminated sheet or film comprising

(2') a layer of impact-modified polymethyl methacrylate, polycarbonate or a molding composition of component (1) as set forth in claim 1

5 and

(3) a top layer of polymethyl methacrylate.

4. A laminated sheet or film as claimed in any of claims 1 to 3 having an overall thickness of from 100  $\mu\text{m}$  to 10 mm.

10

5. A laminated film comprising, in this order,

(1') a substrate layer comprising a molding compound of component (1) as set forth in claim 1, ABS, polycarbonate, polybutylene terephthalate, polyethylene terephthalate, polyamide, polyetherimide, polyether ketone, polyphenylene sulfide, polyphenylene ether or blends thereof, having a layer thickness of from 90 to 990  $\mu\text{m}$ ,

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(3') a transparent top layer comprising polymethyl methacrylate, high-impact polymethyl methacrylate, ABS, polycarbonate, polyethylene terephthalate, styrene-acrylonitrile copolymers, polyamide, polyether sulfone or polysulfone, having a layer thickness of from 10 to 100  $\mu\text{m}$ ,

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it being possible for the substrate layer to comprise special-effect colorants and comprising them if the substrate layer and the top layer are composed of the same molding compounds, and the overall thickness of the laminated film being from 100 to 1000  $\mu\text{m}$ .

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6. A laminated film as claimed in claim 5, additionally comprising between the top layer and the substrate layer

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- (2") an interlayer of polymethyl methacrylate, high-impact polymethyl methacrylate, ABS, polycarbonate, polyethylene terephthalate, styrene-acrylonitrile copolymers, polyamide, polyether sulfone or polysulfone, which comprises special-effect colorants and has a layer thickness of  
5 from 50 to 400  $\mu\text{m}$ .
7. A laminated film as claimed in claim 5 or 6, additionally comprising, on the outer surface of the substrate layer,
- 10 (0) an adhesion layer comprising an adhesion promoter having a layer thickness of from 5 to 100  $\mu\text{m}$ .
8. A laminated sheet or film as claimed in any of claims 1 to 7, the ratio of the MFI values of the individual components of the laminated sheet or film being  
15 not more than 3:1.
9. A process for producing a laminated sheet or film as claimed in any of claims 1 to 8 by adapter coextrusion or die coextrusion of components (0) and/or (1)/(1') and/or (2)/(2')/(2") and/or (3)/(3'), the overall laminate being  
20 produced in a single-stage process.
10. A process for producing a laminated sheet or film as claimed in any of claims 1 to 8 by laminating films or sheets of components (0) and/or (1)/(1') and/or (2)/(2')/(2") and/or (3)/(3') onto one another in a heatable roll nip.  
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11. The use of a laminated sheet or film as claimed in any of claims 1 to 8 for producing a molding.
12. A process for producing a molding from a laminated sheet as claimed in  
30 claim 1, claim 2 or any claim which relates back to these claims by

thermoforming the laminated sheet.

13. A process for producing a molding from a laminated sheet or film as claimed in claim 3, 5, 6, 7 or any of the claims which relate back to these claims by thermoforming the laminated sheet or film and backspraying with component (1) as set forth in claim 1 or with a polyurethane foam.
14. A process for producing a molding from a laminated film as claimed in any of claims 5, 6, 7, or 8, relating back to any of these claims, by backspraying or back-casting the laminated film with component (1') as set forth in claim 5 or with a polyurethane foam, it being possible for the laminated film to be thermoformed beforehand, or by laminating a molding comprising the component as set forth in claim 5, or a polyurethane foam, with the laminated film.
15. A molding comprising a shaped laminated sheet as claimed in claim 1, claim 2 or any claim which relates back to these claims.
16. A molding comprising a shaped laminated sheet or film as claimed in any of claims 3, 5, 6, 7 or any claim relating back to these claims, which is back-sprayed or back-cast with component (1') as set forth in claim 5 or with a polyurethane foam, or where a molding comprising component (1') as set forth in claim 5, or a polyurethane foam, is laminated with the laminated film.
17. A molding as claimed in claim 12 or 13 in the form of an automotive exterior bodywork component.
18. A laminated sheet or film as claimed in any of claims 1 to 8, wherein a transport protection film is applied to the outside of the top layer (3) or (3'), respectively.